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Evaluating the Impacts of Changing Water Quality on Corrosion Control

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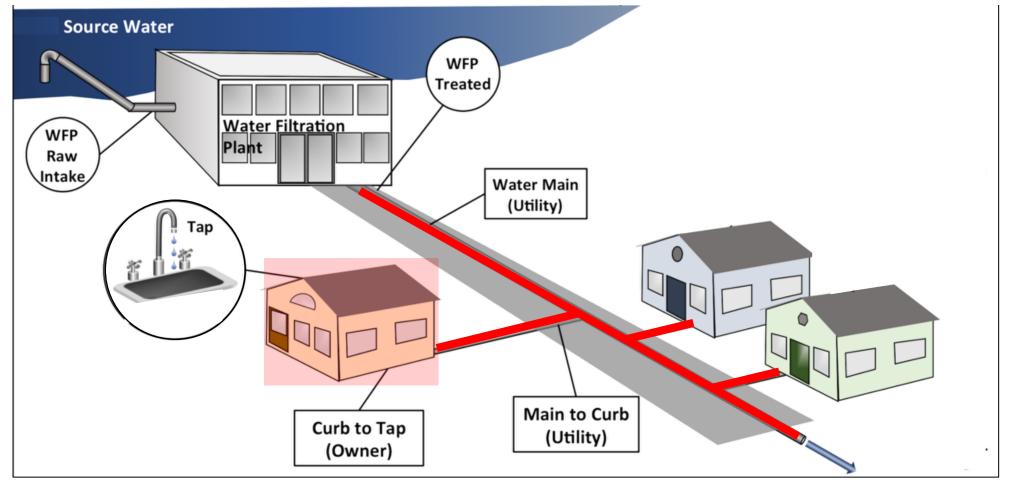
PRESENTATION OUTLINE

- Corrosion in the distribution system
 - $_{\odot}$ What is corrosion in the distribution about?
 - $_{\odot}$ Why does it matter?
 - $_{\odot}$ What affects corrosion?
 - $_{\odot}$ How is corrosion potential evaluated?
 - Case study: Tottenham, New Tecumseth, Ontario
 - $_{\odot}$ How is the corrosion control chemical selected?
 - Case study: Windsor Lake Water Treatment Plant, City of St. John's, Newfoundland

WHAT IS CORROSION IN THE DISTRIBUTION ABOUT?

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Corrosion in the distribution system refers to transfer of metal from pipe walls into the bulk water that results in elevated metal concentrations in drinking water



Adapted from USGS 2015, https://www.usgs.gov/media/images/idealized-diagram-a-public-water-supplys-water-distribution-system

WHY DO WE CARE?

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- Main concerns of corrosion in distribution piping:
 - $_{\odot}$ Loss of pipe mass leading to structural weakening of pipes, watermain leaks
 - $_{\odot}$ Tuberculation limiting the hydraulic capacity of pipes and increase head loss
 - Release of metal ions leading to coloured water, T&O issues, and or/elevated lead and copper



1. Structural weakening of pipes



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2. Tuberculation



Release of metal ions

- Water Quality Parameters
 - \circ pH, alkalinity
 - $_{\odot}$ Dissolved inorganic carbon
 - \circ Hardness
 - o Oxidants (e.g. dissolved oxygen, chlorine, chloramine)
 - $_{\odot}$ Anions (e.g. sulfide, chloride, sulfate)
 - \circ Temperature
- Pipe material
- Hydraulic conditions

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Corrosion index	Calculation Method	Application
Langelier Saturation Index	$LSI = pH_{measured} - pH_{calulated saturation}$	 Historically commonly used corrosion indices,
Calcium Carbonate Precipitation Potential	Iterative calculations	which estimate the extent of calcium carbonate precipitation and dissolution in the distribution
Ryznar Stability Index	$RSI = 2 \ pH_{calulated \ saturation} - pH_{measured}$	 system Have not been found to strongly correlate with actual corrosion rates
Corrosive (dissolution)	HCO ₃ -(aq) + Ca ²⁺ (aq) CaCO ₃ (s)	Scaling (precipitation) CaCO ₃ (s)



Corrosion Index	Calculation Method	Application
Chloride to Sulfate Mass Ratio (CSMR)	$CSMR = \frac{Cl^{-}(\frac{mg}{L})}{SO_{4}^{2-}(\frac{mg}{L})}$	Correlated with lead release, where lead solder or partially replaced lead pipe is used to connect copper pipes
<image/>	Lead (Pb) Pb $^{2+}$ PbSO ₄ (s) SO ₄ Composition of the second sec	Copper (Cu)

CORROSION METAL RELEASE MODELS



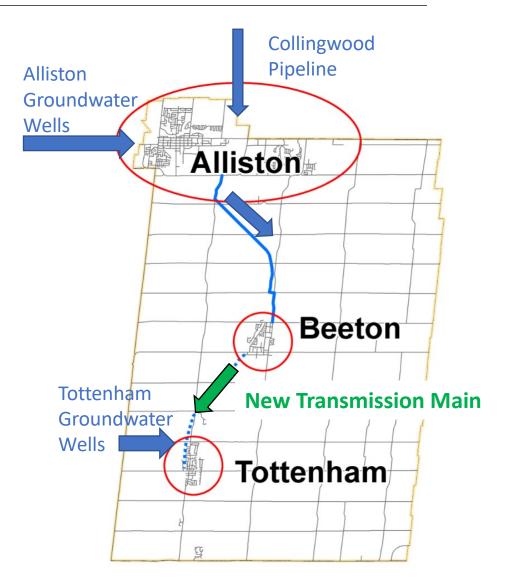
Corrosion Index	Calculation Method	Application
Red water (iron release model)	$Fe = \frac{0.0132 \ (Cl)^{0.485} Na^{0.561} SO_4^{2-0.118} DO^{0.967} T^{0.813} HRT^{0.836}}{10^{1.321} Alk^{0.912}}$	Alternative indicators of corrosion
Lead release model	$Pb = (CF)1.027^{T-25}Alk^{0.677}pH^{-2.726}Cl^{1.462}SO_4^{2-0.228}$	potential, developed from pipe loop studies
Copper release model	$Cu = T^{0.72} Alk^{0.73} p H^{-2.86} SO_4^{2-0.1} SiO_2^{-0.22}$	



https://doi.org/10.1002/awwa.1127

TOTTENHAM - INTRODUCTION

- Existing Tottenham water system is fed by four ground water wells
- New Tottenham Transmission Main is being connected to the Beeton water supply (predominantly surface water from Collingwood)
- Tottenham groundwater wells will remain as a backup supply for the Town
- Tottenham groundwater will be blended with Beeton supply in the event of very high demands
- Significant changes in water source and treatment can change the corrosivity of the water
- During the switch-over to the Beeton water supply, process changes may be required to accommodate varying water quality between systems



METHOD

- Water quality tests were conducted on samples collected at locations that represent water from Beeton (predominantly Georgina Bay water) and Tottenham (ground water) that may be blended in the future
- Blend characteristics were determined based on:
 - o mass balance calculations for conservative parameters (e.g. chloride)
 - $_{\odot}$ AWWA TetraTech Rothberg Tambuirini and Winsor (RTW) Model for pH

	Water Source	Blend Percentage						
	Tottenham	100%	75%	50%	25%	0%		
	Beeton	0%	25%	50%	75%	100%		
рН		8.14	8.13	8.11	8.08	8.04		
Alkalinity	CaCO ₃ mg/L	205	177	150	122	94		
Calcium	CaCO ₃ mg/L	105	85	66	47	28		
Chloride	mg/L	58	47	36	25	14		
Sulfate	mg/L	0.45	2.92	5.4	7.9	10.34		

Corrosion	Guidelines/Target	Water Source	Blend Percentage				
indices/metal release model		Tottenham	100%	75%	50%	25%	0%
		Beeton	0%	25%	50%	75%	100%
Calcium Carbonate Precipitation Potential (CCPP)	Scaling (protective): >0 Passive: 0 to -5 Mildly corrosive: -5 to -10 Corrosive: <- 10		14.4	8.9	4.4	0.5	-2.7
Langelier Saturation Index (LSI)	Positive value: deposition of $CaCO_3$ Negative value: dissolution of $CaCO_3$ Recommended to be -0.5 to 0.5		0.57	0.45	0.28	0.05	-0.31
Ryznar Stability Index (RSI)	Scaling (protective): >7 Passive: 5 to 7 Corrosive: <5		6.99	7.23	7.54	7.98	8.67

RESULTS

Corrosion indices/metal release model		Water Source	Blend Percentage					
	Guidelines/Target	Tottenham	100%	75%	50%	25%	0%	
		Beeton	0%	25%	50%	75%	100%	
Chloride-Sulfate Mass Ratio (CSMR)	No concern: < 0.2 Significant concern: 0.2 to 0.5 Serious concern: >0.5 and <50 mg/L alkalinity		130	16	7	3	1	
Iron release (mg/L)	Aesthetic objective: ≤ 0.3 mg/L		0.07	0.09	0.10	0.09	0.07	
Lead release (ug/L)	≤ 10 µg/L		4.9	2.4	1.3	0.6	0.2	
Copper release (mg/L)	Aesthetic objective: ≤ 1.0 mg/L Maximum acceptable concentration (MAC): 2 mg/L		0.55	0.70	0.77	0.82	0.87	

- CSMR is applicable for lead-copper connections
- Town has advised that lead piping has not been found in previous studies. Presence of lead pipes in unknown
- Lead testing conducted by the Town in 2008, 2011, 2014, and 2017 showed lead levels (0-5 ug/L) below the allowable concentration (10 ug/L)
- The calibrated lead release model indicated that the expected lead levels in all blends (0-5 ug/L) are below the allowable concentration (10 ug/L).
- More importantly, the lead release model indicates the expected lead release decreases with increasing percentage of Beeton water.

LEGACY MANGANESE

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- Legacy manganese is manganese that accumulates in the distribution system and leach out when the system destabilizes
- Release of legacy manganese can lead to coloured water events and exposure to regulated heavy metals that co-accumulate with manganese
- Legacy accumulation in the Tottenham distribution is possible given that the groundwater has >0.02 mg/L manganese



AWWA Research Webinar May 2021

- Prior and after the switchover, conduct flushing of the distribution system. Unidirectional flushing at velocities greater than 1.8 m/s is preferred.
- Maintain chlorine residual above 0.4 mg/L throughout the distribution system
- Regular monitoring of lead, copper, manganese, iron and other relevant water quality parameters before and after transitioning from Tottenham to Beeton water

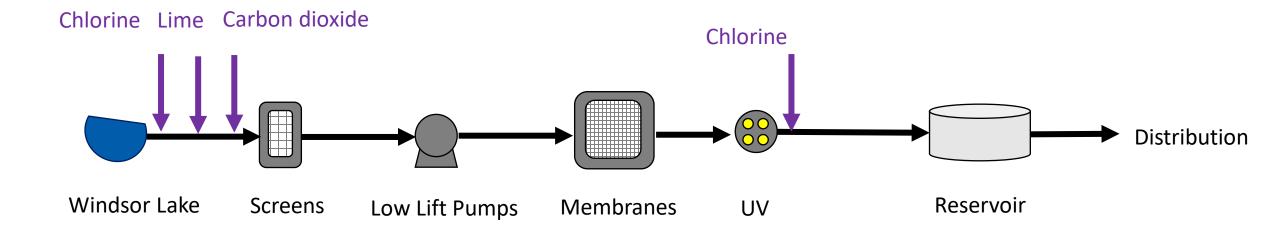
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WINDSOR LAKE WTP INTRODUCTION



- Addition of lime prior to membrane filtration poses O&M issues with the membranes
- Target alkalinity (35 mg/L) and pH (8) cannot be met



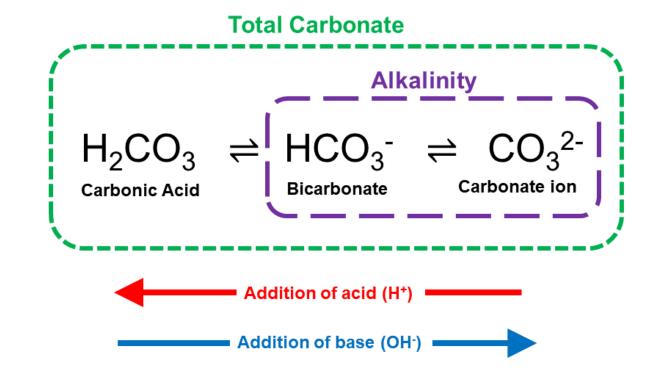
• pH

 High pH typically reduces the solubility and by extension, the release of metals from pipes

High pH can lead
 excessive calcium
 carbonate precipitation

Alkalinity

 Measure of the capacity to resist pH



- 1. Use AWWA RTW model to estimate require chemical doses to meet target pH and alkalinity. Compare to previously conducted bench-scale testing results
- 2. Compare pros and cons, capital and operational costs for each chemical

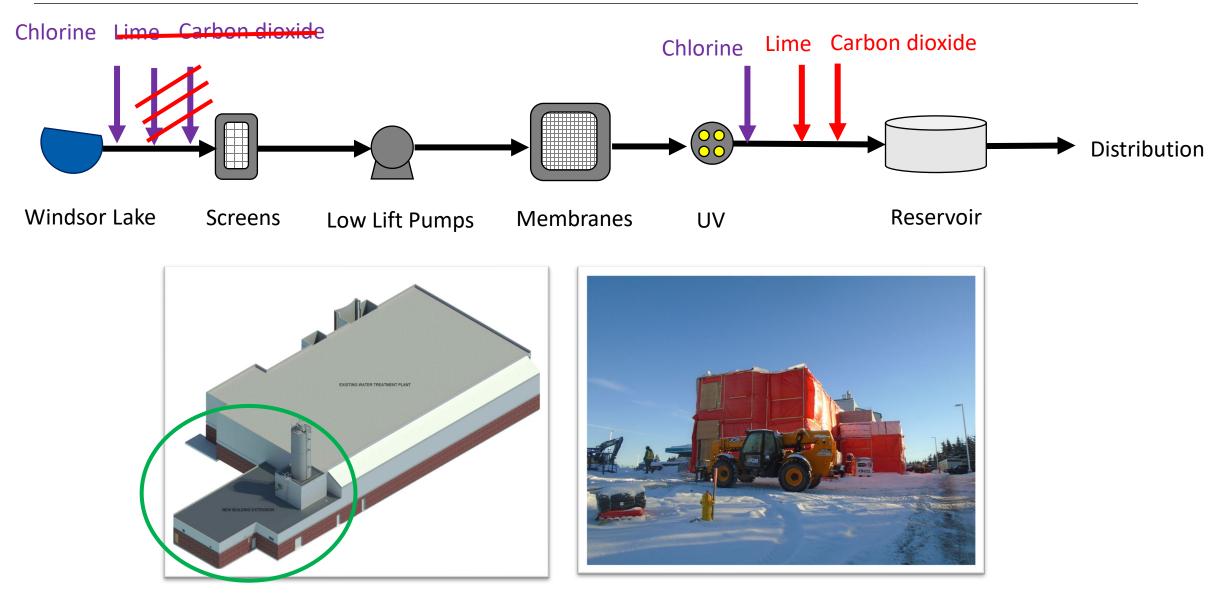
Chemical	Alkalinity added (+) or consumed (-) (mg/L CaCO ₃ per mg/L of chemical)
Lime	+1.35
Caustic Soda	+1.25
Soda Ash	+1.94
Baking Soda	+0.6
Chlorine	-1.41

Chemical	Chemical Reaction	Purpose	Advantages (+) Disadvantages (-)	Estimated dose (mg/L)	Annual chemical cost (\$)	Process equipment cost (\$)
Hydrated Lime Ca(OH) ₂	Ca(OH) ₂	<u>Increase</u> pH	 + Operator familiarity with chemical - Low solubility - Often results in higher turbidity in finished water - High attraction to moisture in atmosphere - Requires dust control - Tendency for scaling/plugging of feed lines 	30	\$0.58M	\$1.08M
Caustic Soda (sodium hydroxide) NaOH	NaOH → Na⁺ + OH⁻		+ Low O&M feed system - Hazardous chemical - High freezing point (14°C)	30	\$1.81M	\$0.7M

Chemical	Chemical Reaction	Purpose	Advantages (+) Disadvantages (-)	Estimated dose (mg/L)	Annual chemical cost (\$)	Process equipment cost (\$)
Soda ash (sodium carbonate) Na ₂ CO ₃	Na ₂ CO ₃ → 2Na ²⁺ + CO ₃ ⁻	<u>Increase</u> pH	 + Nonhazardous chemical + Relatively easy to handle and dose - Requires dust control 	40	\$1.60M	\$1.03M
Baking soda (sodium bicarbonate) NaHCO ₃	NaHCO ₃	+ Add carbonate	+ Nonhazardous chemical - Requires dust control	60	\$1.81M	\$1.05M
Carbon dioxide CO ₂	$CO_2 + OH^- →$ HCO ₃ ⁻	Decrease pH + Add carbonate	+ Useful for trimming pH when used with other chemicals like hydrated lime and caustic soda	12-30	\$0.5-1M	N/A

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WINDSOR LAKE WTP



- Significant changes in water source and treatment can change the corrosivity of the water
- Calcium carbonate based indices have not been found to strongly correlate with actual corrosion rates
- Metal release models are useful tools to predict corrosion in the distribution system
- Legacy manganese needs to be considered as part of corrosion control
- Chemical selection for alkalinity and pH adjustment depends on carbonate chemistry, costs, and O&M needs